

18/4-18

Föreläsning 7

• Nyquist stability theory relation between open and closed-loop.

• Argument variation principle

• Stability by Nyquist

$$\dot{x}(t) = Ax(t), \quad x_0 \quad (\text{Socratic})$$

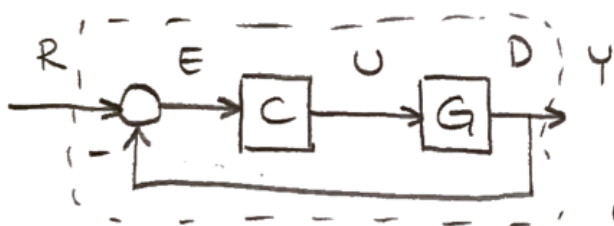
$$x(t) = e^{At} \cdot x_0 \quad \Big|_{u=0}$$

state transition matrix

~~✱~~

Avoid mixing it with similarity state-transform.

$$\tilde{x}(t) = Tx(t)$$



(Socratic)

$$G_c = T$$

$$T(s) = \frac{Y(s)}{R(s)} = \frac{L(s)}{1 + L(s)}$$

+

$$S(s) = \frac{Y(s)}{D(s)} = \frac{1}{L(s) + 1}$$

$$1 - T = S$$

PID

(socratic)

$$C(s) = K_p + \frac{K_i}{s} + K_d s$$

P I D

dynamics structured

not state! It is output.

$$U(s) = C(s) E(s) = C(s) (R(s) - Y(s))$$

output feedback

output

there is no state.

1. Nyquist stability theory

Aim: With the loop transfer function

$L(s) = G(s)C(s)$ decide whether the closed-loop is stable or not,

$$T(s) = G_c(s)$$

1) Relation $T(s) \leftrightarrow L(s)$

2) How to do?

Note, nyquist stat. criteria fits into the controller tuning methods (L6)

1) Heuristics

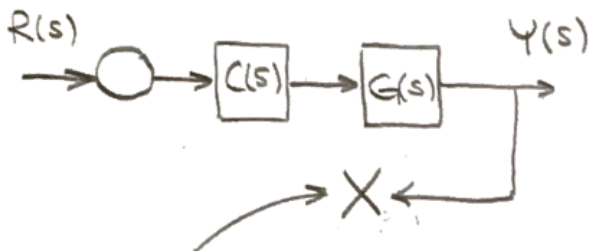
2) Guaranteed stability

2. Relation between open and closed-loop

Blockdiagrams



OPEN

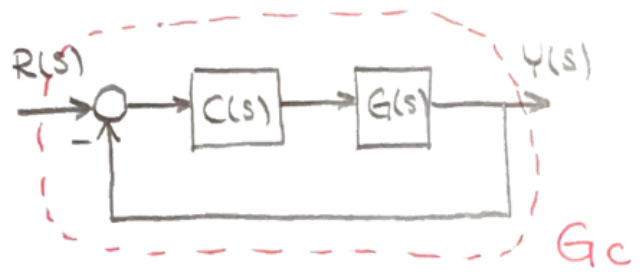


opening the loop.

$$f(s) = L(s) + 1 = \frac{b(s) + a(s)}{a(s)}$$

return ratio.

CLOSED

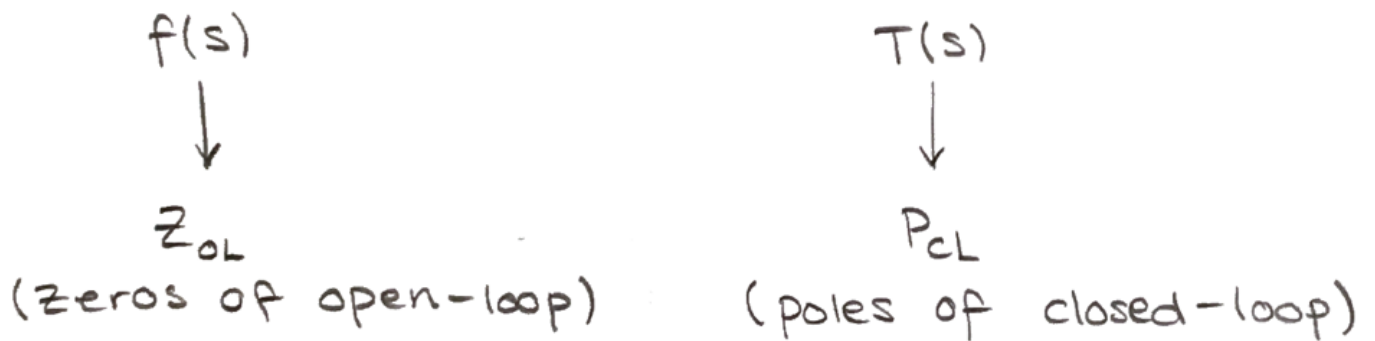


$$T(s) = G_c(s) = \frac{L(s)}{1 + L(s)} = T$$

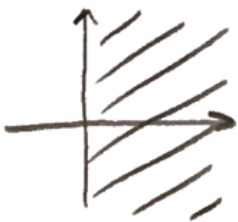
$$= \frac{G(s)C(s)}{1 + G(s)C(s)} = \frac{b(s)}{a(s) + b(s)}$$

$$L(s) = \frac{b(s)}{a(s)}$$

Pole polynomial for $T(s)$ is identical to the zero polynomial of $f(s)$



We aim at finding z_{OL} over RHP



Need for searching over RHP:

Technique to seek is by means of Cauchy integral criteria.

Argument variation principle

Theorem Let $f(s)$ be holomorphic on D (domain) closed by a (piecewise smooth curve) Γ (no poles, no zeros on Γ) except a finite number of zeros and poles. Then,

$$z - p = w$$

where z/p is the total # of zeros/poles of $f(s)$ over D .

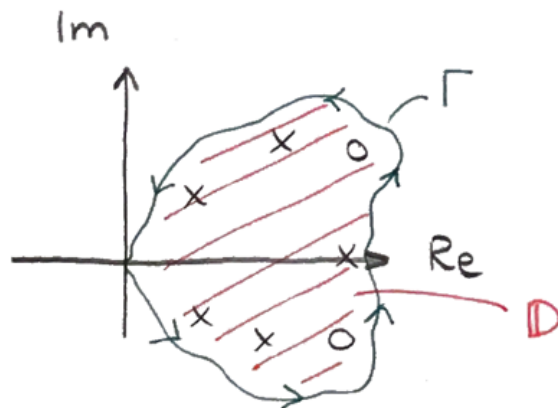
Including multiplicities (repeated poles/zeros at the same location)

And w is a winding/encirclement # around origin of \mathbb{C} .

We will select D to be the RHP.

e.g.

domain
for $f(s)$



o - zeros

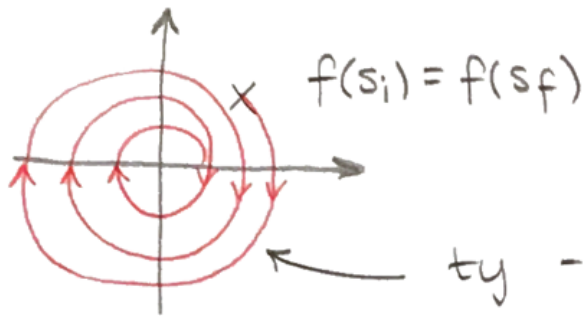
x - poles

Γ tipping direction CCW positive \oplus

$$z - p = 2 - 5 = -3$$

spinning/winding around the origin

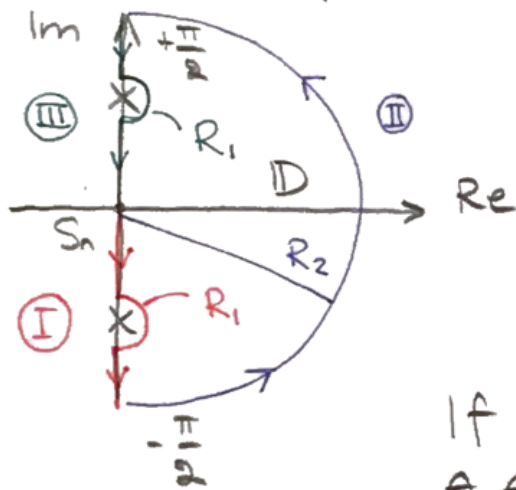
$$f(s) \quad s \in \mathbb{D}$$



ty -3 är negativ byter man håll på varven.

Let's map RHP $\leftarrow \mathbb{D}$

How to define \mathbb{D} ?



x - poles

Nyquist contour

step I:

$$s = -i \cdot \omega$$

If there is a pole $R_1 e^{i\theta}$ $R_1 \rightarrow 0$
 $\theta \in \left[+\frac{\pi}{2}, -\frac{\pi}{2} \right]$

Step II:

$$s = R_2 e^{i\theta} \quad \theta \in \left[-\frac{\pi}{2}, +\frac{\pi}{2} \right], \quad R_2 \rightarrow \infty$$

Step III:

$$s = +i\omega \quad \omega(\infty, 0]$$



Note,

$$Z_{OL} - P_{OL} = W_{OL}$$

$$P_{CL} = Z_{OL}$$

$$P_{CL} - P_{OL} = W_{OL}$$

$$P_{CL} = \underbrace{W_{OL} + P_{OL}}$$

open-loop \Rightarrow closed-loop

3. Stability by Nyquist

Theorem The closed-loop is asymptotically input-output stable (no $P_{CL} = 0$ at RHP)

$$P_{CL} = W_{OL} + P_{OL}$$

where P_{CL} is the number of closed-loop poles.

P_{OL} is # of open-loop poles.

W_{OL} is the encirclement of $f(s)$ around Φ

Nyquist simplified further the stability theorem as $P_{OL} = 0$ (no unstable open-loop poles), $f(s) = L(s) + 1$

encircling origin Φ

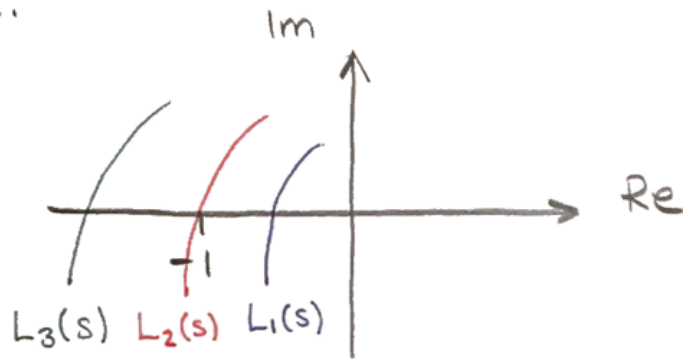


w/ $L(s)$ encircle -1 .

Theorem (Simplified Nyquist theorem)

The closed-loop is asymptotically stable (input-output) iff $P_{CL} = 0$ and if $P_{OL} = 0$ then $P_{CL} = \omega_{OL} = 0$
 ω_{OL} is the encirclement around (real) -1 point.

e.g.



$L_1(s) \Rightarrow \omega_{OL} = 0$ if $P_{OL} = 0$
 $\Rightarrow P_{CL} = 0 \Rightarrow$ stable

$L_2(s) \Rightarrow$ marginally stable
(Lyapunov stable)

$L_3(s) \Rightarrow \omega_{OL} \neq 0 \Rightarrow P_{CL} \neq 0$
unstable

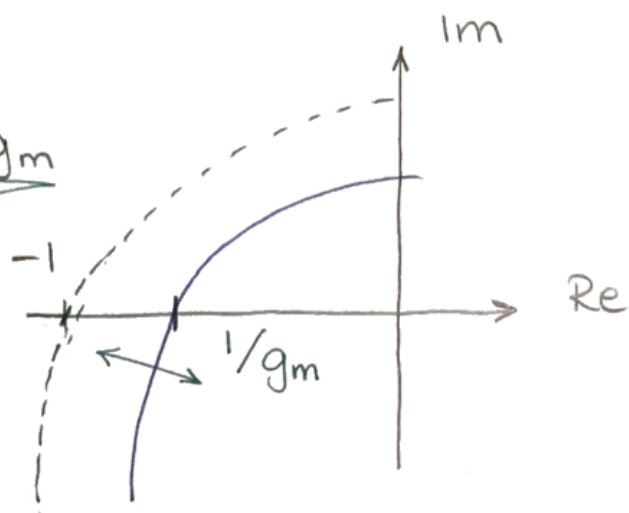
We looked at $L(s)$ and concluded stability for $T(s)$ (closed-loop)

What if a closed-loop is stable, how much surplus/margin we have before getting unstable

1) Gain margin

$$0 < g_m < \infty$$

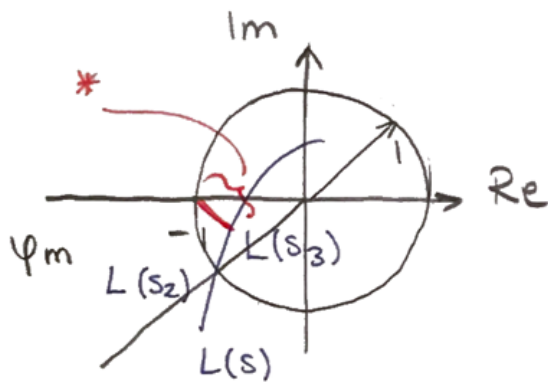
$$g_m L(s_1) = |L(s_1)| e^{i\varphi(s_1)} \quad \underline{g_m}$$



2) Phase margin

$$L(s_2) = |L(s_2)| e^{i(\varphi(s_2) + \varphi_m)}$$

← phase margin



3) Stability margin

⊛ stability margin, s_3

$$\min_s |L(s) - (-1)| = \min_s \underbrace{|L(s) + 1|}_{f(s)}$$

⇔

$$\max_s \left| \frac{1}{L(s) + 1} \right| = \max_s |S(s)|$$

↑ sensitivity function