

9/4-18

Föreläsning 5

- 1) From state-space to transfer function
 - 2) Solution to the LTI state-space
 - 3) Stability
 - 4) Controllability
 - 5) Observability
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- 1) From state-space to transfer function

$$G(s) = \frac{Y(s)}{U(s)} = \frac{b(s)}{a(s)}$$

$$\begin{cases} \dot{x}(t) = Ax(t) + Bu(t) & x_0 = 0 \\ y(t) = Cx(t) + Du(t) \end{cases}$$

$$\mathcal{L}(\dot{x}(t) = Ax(t) + Bu(t))$$

$$(sI - A)X(s) = BU(s)$$

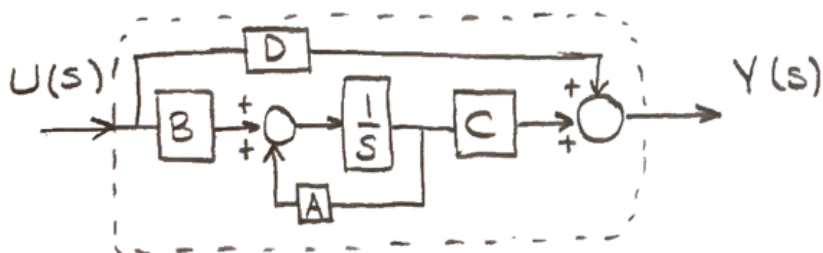
$$X(s) = BU(s)(sI - A)^{-1}$$

$$\mathcal{L}(y(t) = Cx(t) + Du(t))$$

$$Y(s) = CX(s) + DU(s)$$

$$Y(s) = (C(sI - A)^{-1}B + D)U(s)$$

$$G(s) = C(sI - A)^{-1}B + D$$



TF above is parametrized by
 (A, B, C, D) .



$x(t) (A, B, C, D)$
 $\tilde{x}(t) (\tilde{A}, \tilde{B}, \tilde{C}, \tilde{D})$

} non-unique
state-space models

Theorem 1:

given two state-space forms (A, B, C, D) and $(\tilde{A}, \tilde{B}, \tilde{C}, \tilde{D})$ with $\tilde{x}(t) = Tx(t)$ ($\exists T^{-1}$) then
 $\tilde{A} = TAT^{-1}$, $\tilde{B} = TB$, $\tilde{C} = CT^{-1}$, $\tilde{D} = D$.
 $(T \in \mathbb{R}^{n \times n}$, non-singular)

T-similarity state transformation matrix

Proof

$$\dot{x}(t) = \frac{d}{dt} (T^{-1} \tilde{x}(t)) = T^{-1} \dot{\tilde{x}}(t) = \underbrace{Ax(t) + Bu(t)}_{T^{-1} \tilde{x}(t)}$$

$$\Rightarrow I \dot{\tilde{x}}(t) = TAT^{-1} \tilde{x}(t) + TBu(t) \quad / \text{pre multiply}$$

$$\dot{\tilde{x}}(t) = \tilde{A} \tilde{x}(t) + \tilde{B}u(t)$$

$TAT^{-1} \quad TB$

$$y(t) = Cx(t) + Du(t)$$

$$y(t) = CT^{-1} \tilde{x} + Du(t)$$

$$y(t) = \tilde{C} \tilde{x}(t) + Du(t)$$

$$\tilde{C} = CT^{-1}$$

Note, T does not influence the direct feedthrough term i.e. $\tilde{D} = D$.

2) Solve the state-equation

$x_0 = x(t=0)$ solve the problem

$$\dot{x}(t) = Ax(t) + Bu(t)$$

$$y(t) = Cx(t) + Du(t)$$

Theorem 2:

For an autonomous LTI state equation

$$\dot{x}(t) = Ax(t), \quad x_0 \neq 0$$

$$x(t) = e^{At} \cdot x_0$$

where $e^{At} = I + At + \frac{A^2 t^2}{2!} + \dots$

matrix exponential.

autonomous / no input - closed-loop system model

Theorem 3:

Given x_0

$$\dot{x}(t) = Ax(t) + Bu(t)$$

$$y(t) = Cx(t) + Du(t)$$

then

$$x(t) = \underbrace{e^{At} x_0}_{\text{homogeneous solution}} + \underbrace{\int_0^t e^{A(t-\tau)} Bu(\tau) d\tau}_{\text{particular inhomogeneous solution part } (u(t))}$$

homogeneous solution

particular inhomogeneous solution part $(u(t))$

Proof

$$\dot{x}(t) = Ax(t) + Bu(t), \text{ pre multiply } e^{-At}$$

$$\underbrace{e^{-At} \cdot \dot{x}(t) - e^{-At} \cdot A \cdot x(t)}_{f \cdot \dot{g} + \dot{f} \cdot g} = e^{-At} Bu(t)$$

$$e^{At} A = (I + At + A^2 \frac{t^2}{2!} + \dots) A = e^{At}$$

$$= (A + A^2 t + A^3 \frac{t^2}{2!} + \dots) = A (I + At + A^2 \frac{t^2}{2!} + \dots)$$

$$e^{-At} \cdot A = A e^{-At}$$

$$\frac{d(e^{-At} x(t))}{dt} = e^{-At} \cdot Bu(t)$$

$$e^{-At} x(t) - I \cdot x_0 = \int_0^t e^{-A\tau} B u(\tau) d\tau$$

$$x(t) = e^{At} x_0 + \underbrace{\int_0^t e^{A(t-\tau)} B u(\tau) d\tau}_{\int_0^t g(t-\tau) u(\tau) d\tau}$$

How to get e^{At} ?

e^{At} - state transition matrix

In the time domain: develop Taylor based

approx $e^{At} \cong I + At + A^2 \frac{t^2}{2!}$

$$\exp\left(\begin{bmatrix} a_{11} & a_{12} \\ a_{21} & a_{22} \end{bmatrix} t\right) \neq \begin{bmatrix} e^{a_{11}t} & e^{a_{12}t} \\ e^{a_{21}t} & e^{a_{22}t} \end{bmatrix}$$

↑ generally speaking

If A is in a diagonal form

$$A_d = \begin{bmatrix} \lambda_1 & & & 0 \\ & \lambda_2 & & \\ & & \ddots & \\ 0 & & & \lambda_n \end{bmatrix} \quad \forall \lambda_n \neq \lambda_j \in \mathbb{C}$$

e.g. $x(t) = e^{A_d \cdot t} x_0 = e^{\begin{bmatrix} \lambda_1 & 0 \\ 0 & \lambda_n \end{bmatrix} t} x_0 = \underbrace{\sum_{j=1}^n e^{\lambda_j \cdot t} x(j)}_{\text{basis function}}$

$$x(j) = e^{\lambda_j t} x_0(j)$$

$$y(t) = Cx(t) = [1 \ 1 \ 1 \ \dots] x(t)$$

$$y(t) = \sum_{j=1}^n e^{\lambda_j t} x_0(j)$$

We solved the state equation analytically:

$$x_0, e^{At}, \int e^{A(t-\tau)} B u(\tau) d\tau$$

$$\Rightarrow x(t)$$

What kind of other analytical properties does it have (stability, controllable, etc.)?

3) Stability

Internal mode stability.

Theorem 4:

Given a continuous LTI state-space (autonomous) system model, $\dot{x} = Ax(t)$, x_0 .

The model is Lyapunov / asymptot stable if eigenvalues of A ($\det(\lambda I - A) = 0$) are having

non-positive real parts $\text{Re}(\lambda_n) \leq 0$

or

strictly negative real parts $\text{Re}(\lambda_i) < 0$

$\forall i = 1 \dots n$

Lyapunov - bounded output

Asymptotic says $\lim_{t \rightarrow \infty} x(t) = 0$

This is an internal stability concept.

Eg $G(s) = \frac{(s-1)}{(s+1)(s-1)}$ stable?

a) $G(s) = \frac{Y(s)}{U(s)} = \frac{1}{s+1} \Rightarrow p = -1$

Input - output wise it is STABLE!

b) $G(s) = \frac{s-1}{s^2-1} \rightarrow$ create controller canon. f.

$\begin{bmatrix} -a_1 & -a_2 \\ 1 & 0 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ 1 & 0 \end{bmatrix} \Rightarrow \text{eig}(A)$

$\dim(x) = 2 \leftarrow s^2 \quad \lambda_{1,2} = \pm 1$

$a(s) = s^2 - 1 = s^2 + a_1 s + a_2$

Internally the system model is UNSTABLE

zero-pole cancellation hides internal unstable mode.

Internal. \longrightarrow input
 output
 stability \longleftarrow ~~stability~~
 generally speaking not true.

$\text{Eig}(A) \not\leftrightarrow$ poles of $a(s)=0$ are not always the same.

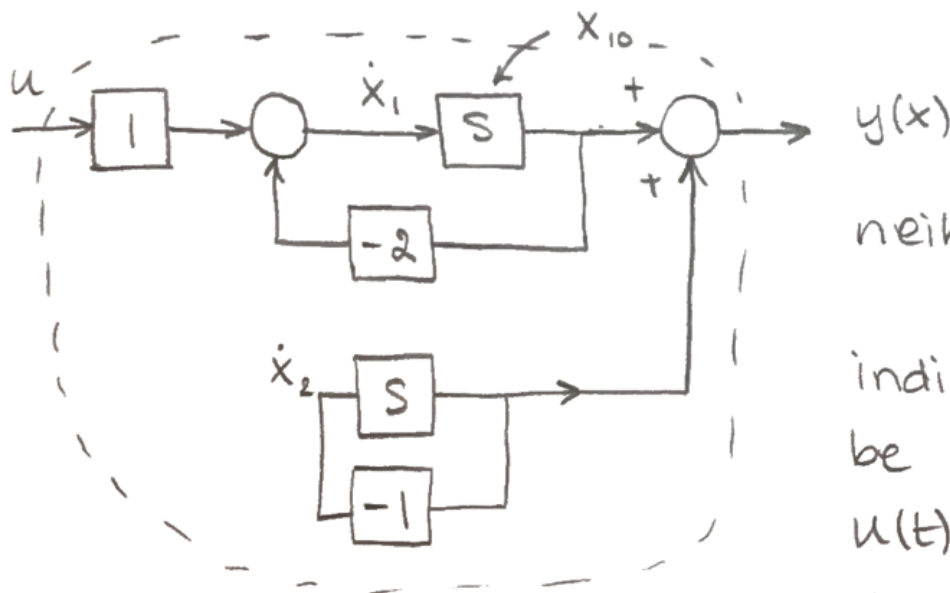
Note, if the state-space is controllable and observable (obs + cont. = minimal state space) then internal stability coincides with input-output

4) Controllability

e.g. Block diagram of $\dot{x}(t) = \begin{bmatrix} -2 & 0 \\ 0 & -1 \end{bmatrix} x(t) + \begin{bmatrix} 1 \\ 0 \end{bmatrix} u(t)$

$$y(t) = [1 \ 1] x(t)$$

$\dim(x) = 2$, SISO



neither directly nor
 $(u \not\rightarrow x_2)$

indirectly $x_2(t)$ can
 be influenced by
 $u(t)$.

$$u \rightarrow x_1 \not\rightarrow x_2$$

x_2 can not be controlled/reached out.

Def. (Reachability $x_0 = 0 \rightarrow x_f \neq 0$ arbitrary).

Given (A, B, C, D) , the LTI system model is said reachable if $\forall x_f = x(t_f)$ terminal state there exists a bounded input $u(t)$, t_f (finite) to travel from $x_0 \rightarrow x_f$.

5) Controllability

Def. (Controllability $x_0 \neq 0 \rightarrow x_f = 0$)

The system model (A, B, C, D) is controllable if for any initial condition $x_0 \neq 0$ there \exists a bounded input sequence and finite time that steers the trajectory to $x_f = 0$.

Controllability and reachability only depends on (A, B)

Theorem 5: A continuous LTI state-space model is controllable / reachable if $\text{rank } R = \dim(x)$

$$R = [B \mid A \cdot B \mid \dots \mid A^{n-1} B]$$

Note, this is the same Kalman rank condition.
e.g.

$$A = \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix}; \quad B = \begin{bmatrix} 1 \\ 0 \end{bmatrix}$$

$$\dim(x) = 2 = n$$

$$R = [B \mid AB \mid \dots \mid \underbrace{A^{2-1} B}_{AB}] = [B \mid AB] = \left[\begin{bmatrix} 1 \\ 0 \end{bmatrix} \mid \begin{bmatrix} -1 & 0 \\ 0 & -2 \end{bmatrix} \begin{bmatrix} 1 \\ 0 \end{bmatrix} \right] =$$

$$= \left[\begin{array}{c|c} \begin{bmatrix} 1 \\ 0 \end{bmatrix} & \begin{bmatrix} -1 \\ 0 \end{bmatrix} \end{array} \right] \quad (\det(R)=0)$$

$$2 = \dim(X) \neq \text{rank } R = 1$$

\Rightarrow is not reach. / cont.